

Electromagnetic Analysis of PCB Parasitic Effects in High Speed Switching Circuits

Francesco Palomba, Technical Support Manager
June 12, 2025



Power Electronics: Trends That Drive Design

Higher Power Densities (power delivered/unit size)



Higher efficiency, shrinking form factor



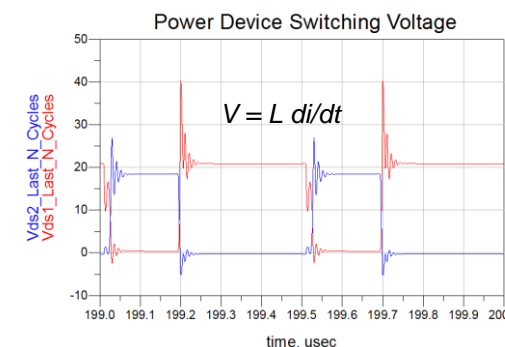
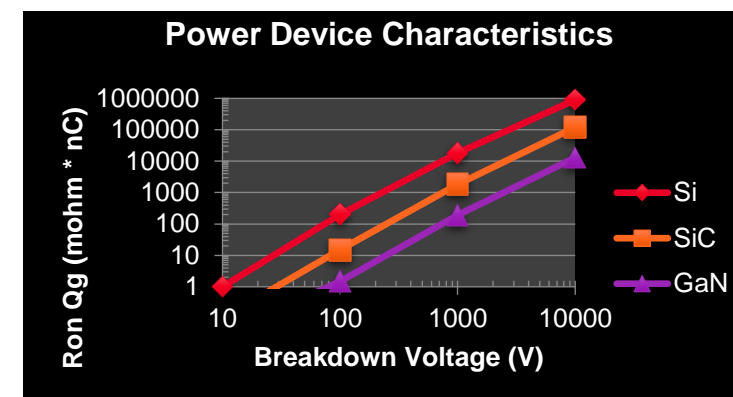
Higher clock frequencies, faster switching edges



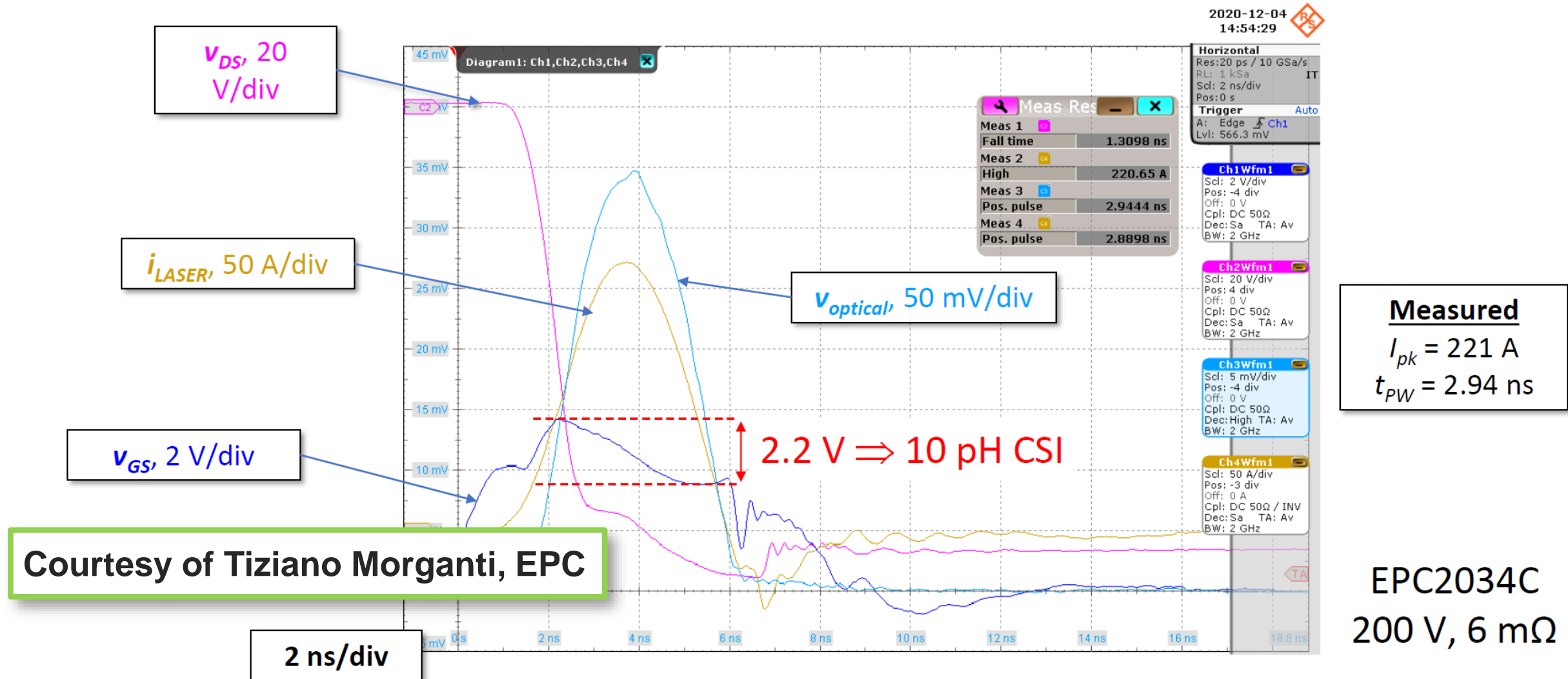
Need for newer device technologies (GaN, SiC)



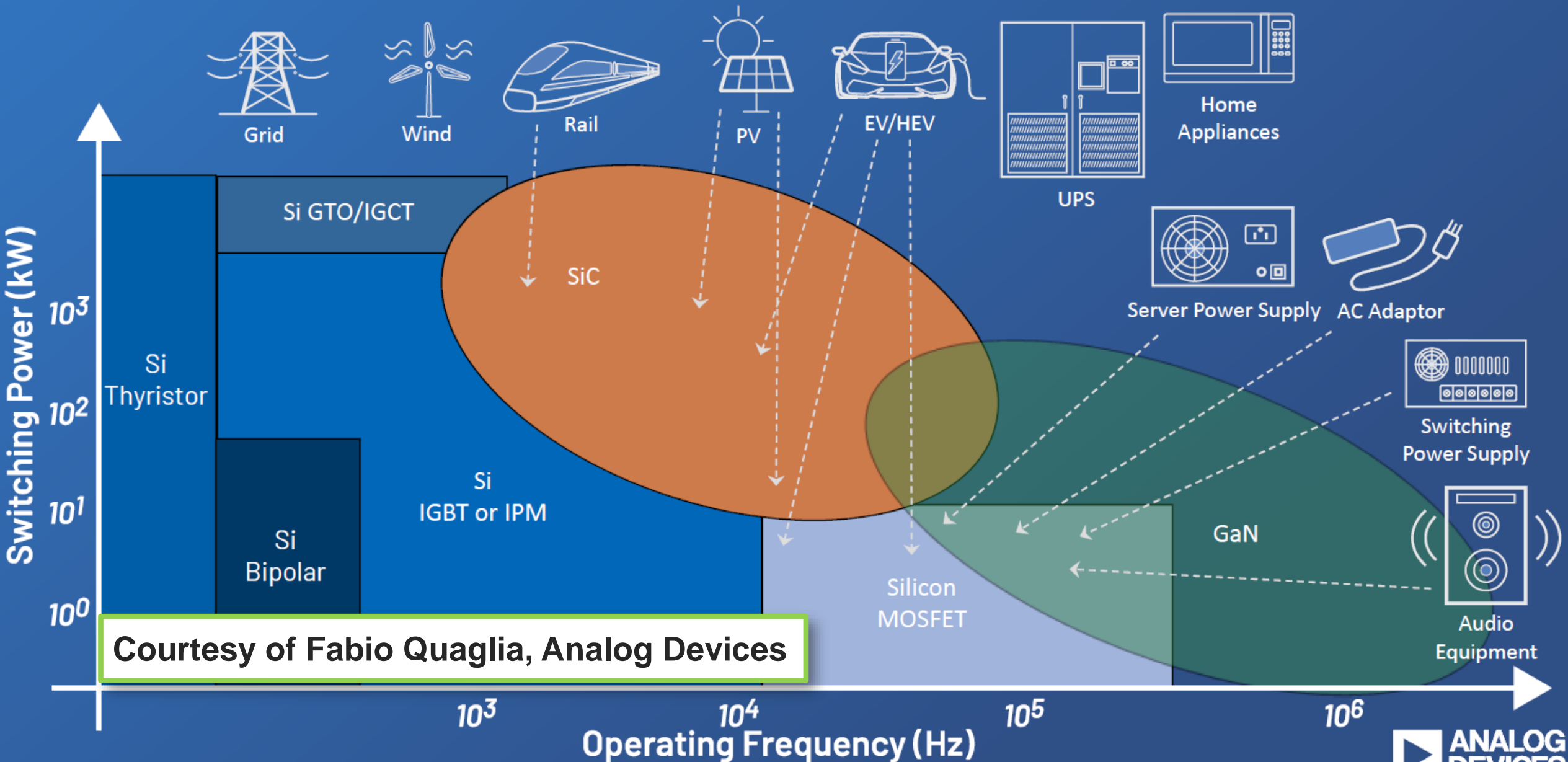
Device models, layout parasitics, EMI, di/dt, thermal mgmt



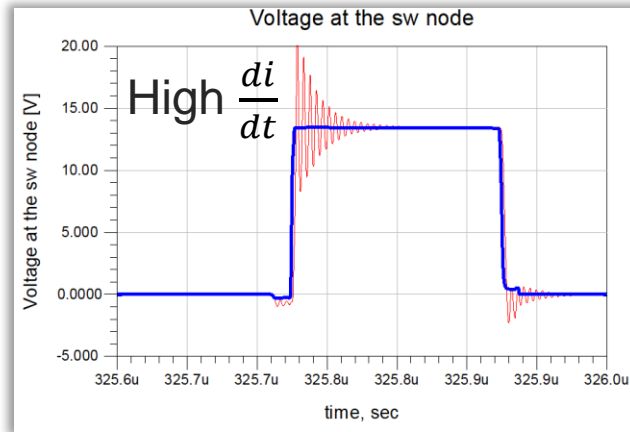
Measurement of EPC9150 215 A laser driver



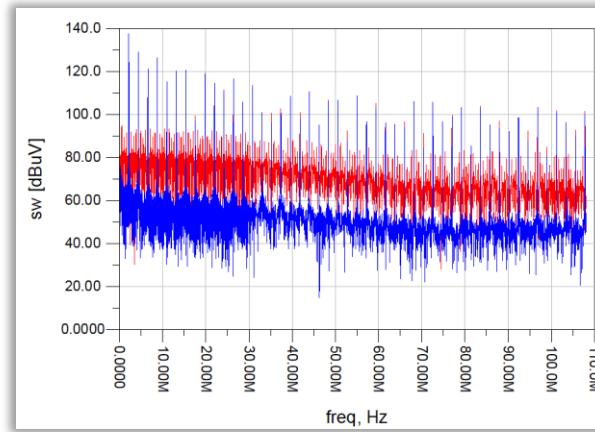
Power Device Competitive Zone



High Frequency Effects



Red with Layout



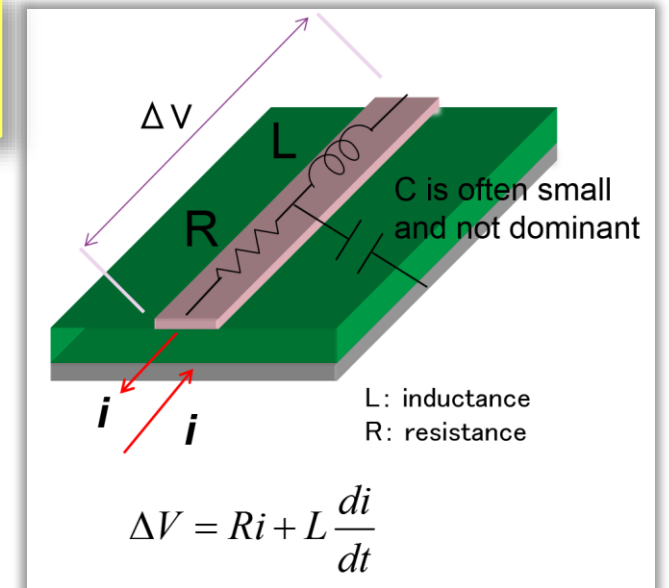
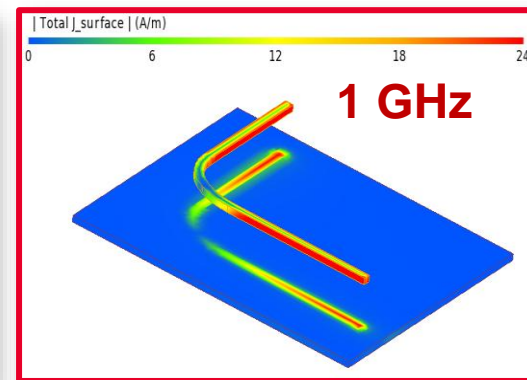
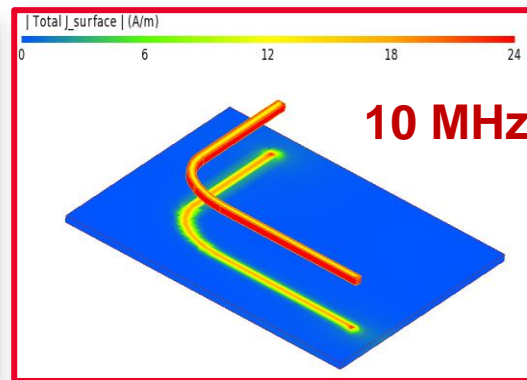
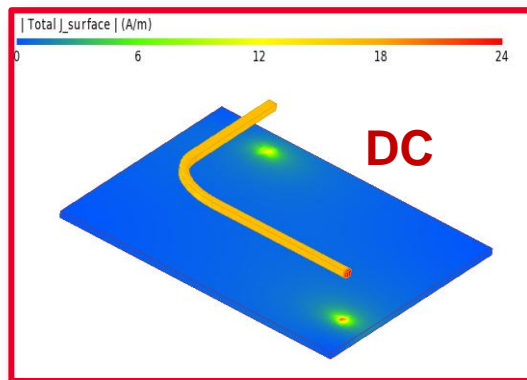
Blue without Layout

Skin Depth vs Frequency		
Frequency	microns	mils
10 KHz	661	26
100 KHz	209	8.2
1 MHz	66	2.6
10 MHz	21	0.8
100 MHz	7	0.3

Skin Resistance vs Frequency	
Frequency	mohms
1 MHz	5
10 MHz	12
100 MHz	40
1000 MHz	224

$$\frac{dI}{dt} \geq \frac{1A}{ns}$$

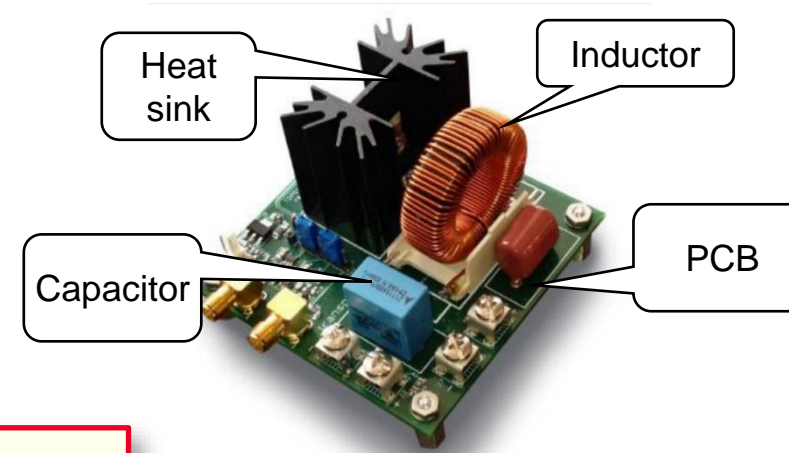
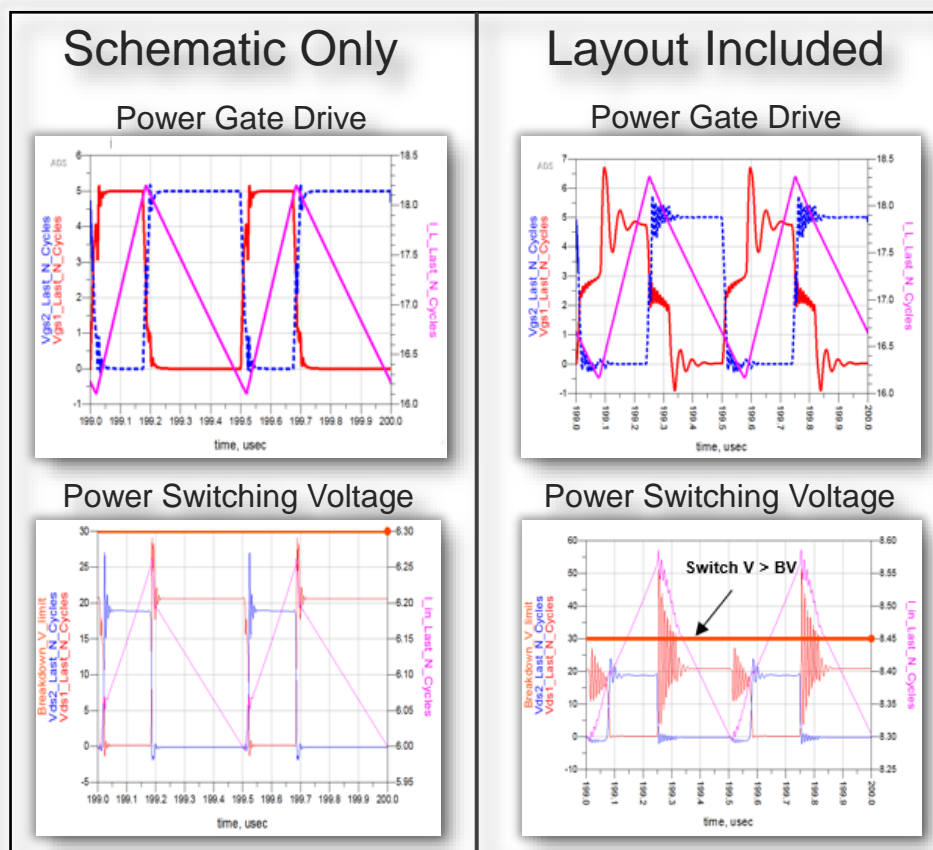
$$\Delta V = R(f)i + L \frac{di}{dt}$$



Challenges SMPS Design

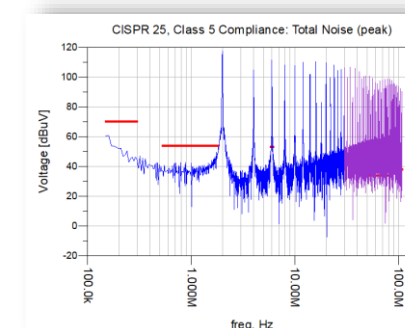
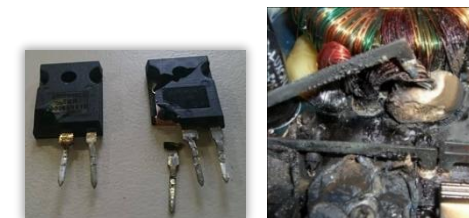
Technical Challenges

- Layout parasitics can cause spikes
- $V_{\text{spike}} = L_{\text{parasitic}} di/dt$

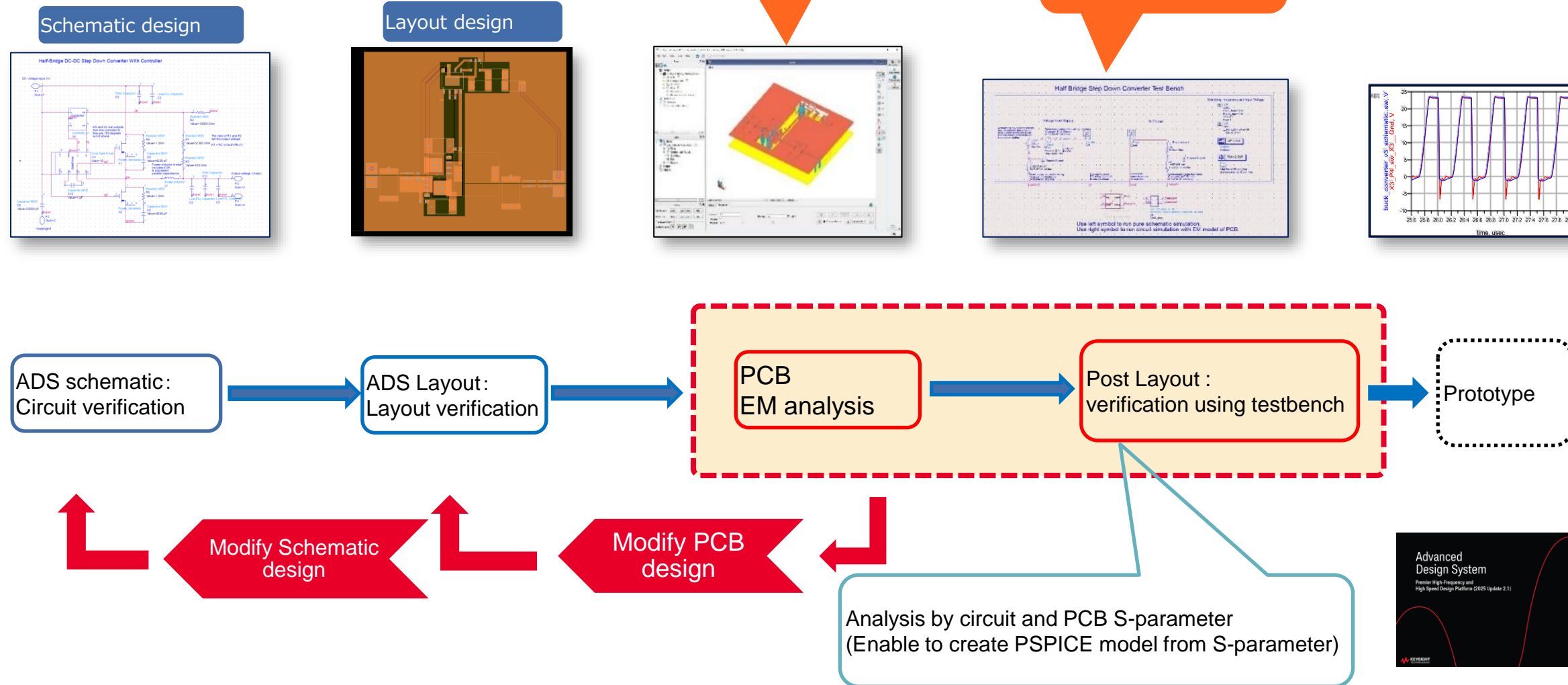


Major risks

- Destruction
- Heat
- Malfunction
- Disruption
- Low Efficiency
- Radiation
- EMC Problems



ADS-PEPro Workflow



3D EM Simulation Technologies

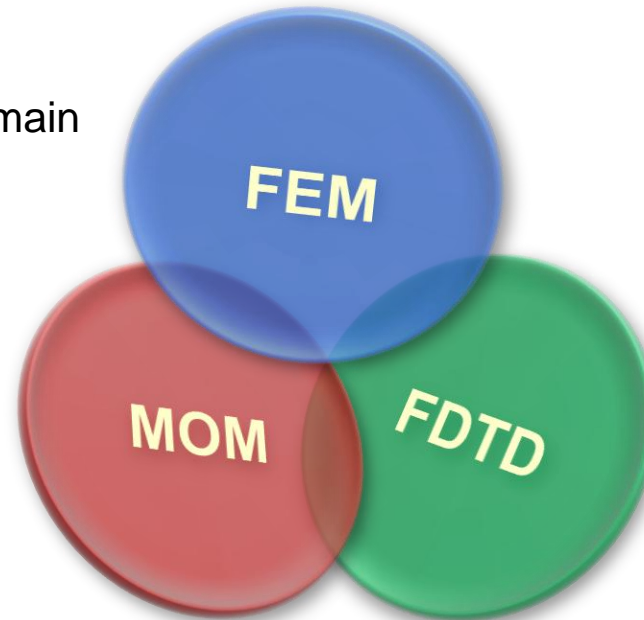


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FEM - Finite Element Method

MOM - Method of Moments

FDTD - Finite Difference Time Domain Method

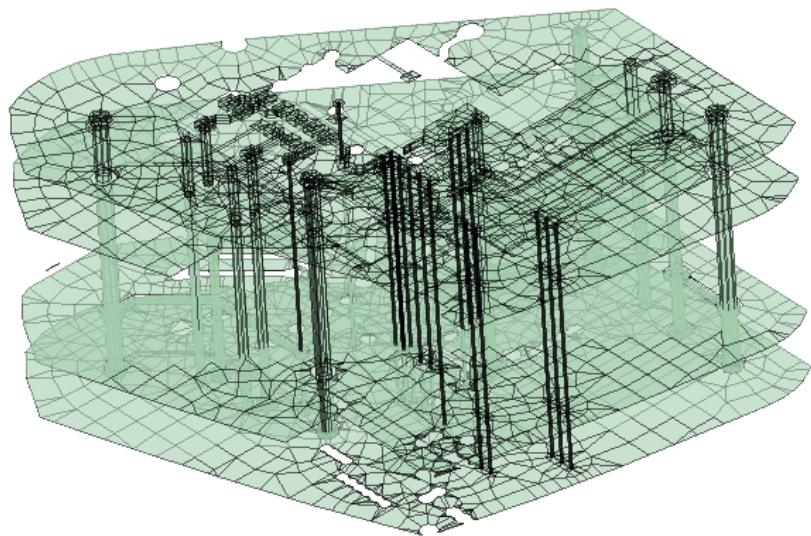


- Restricted 3D Structures
- Frequency Domain
- Full-Wave and Quasi-Static Simulations
- Dense & Compressed Matrix Solvers
- Multiport Simulations at no Additional Cost
- High Q
- ADS UI

- Arbitrary 3D structures
- Frequency Domain
- Full Wave EM Simulations
- Direct, Iterative Solvers
- Multiport Simulations at no Additional Cost
- High Q
- ADS or EMPro UI

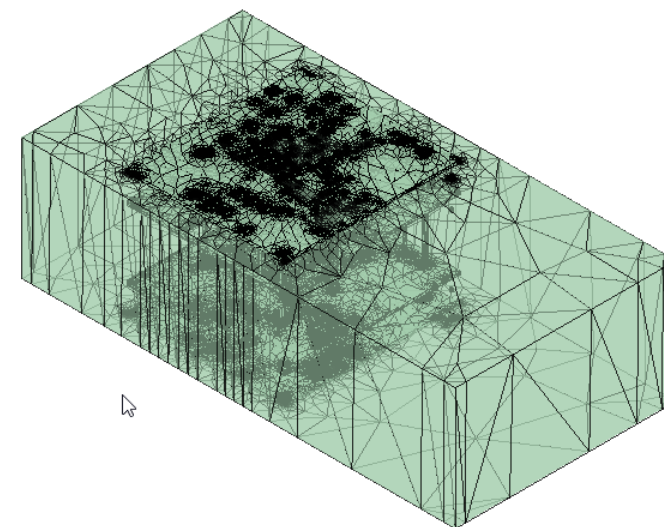
- Arbitrary 3D structures
- Time Domain
- Full Wave EM Simulations
- Handles much larger and complex problems (e.g., complete mobile phone)
- Each port requires separate simulation
- GPU based hardware acceleration
- EMPro UI

Electromagnetic Simulation Results



1 MoM

- Planar Mesh only for conductors
- Pre-computed mesh
- It solves for currents and voltages
- It provides S-parameters, Current Density and Far Field



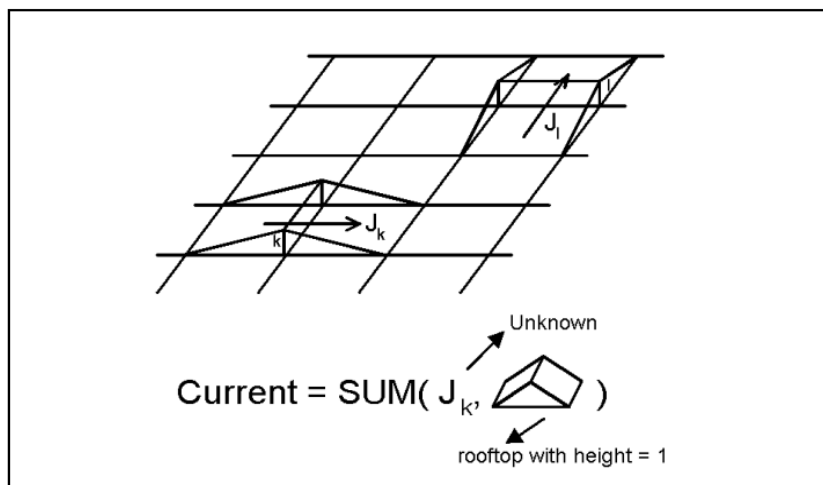
2 FEM

- Volume mesh for the full geometry
- Mesh refinement
- It solves for E and H
- It provides S-parameters, Near Field, Far Field

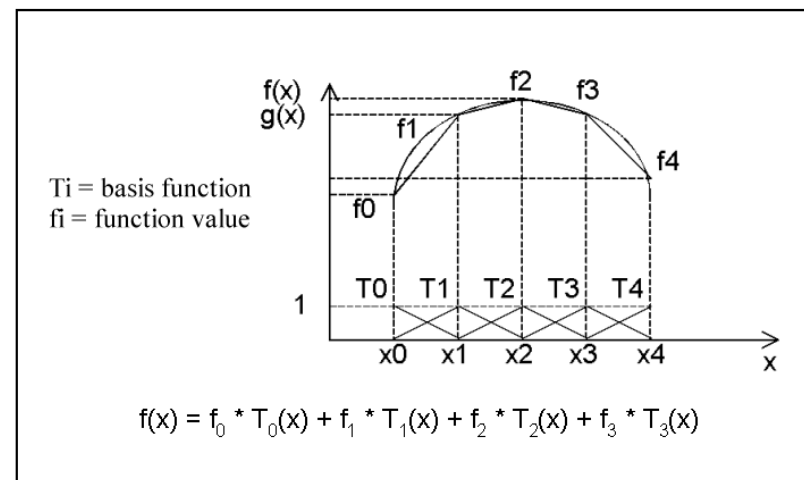
Method of Moments

Basis Functions

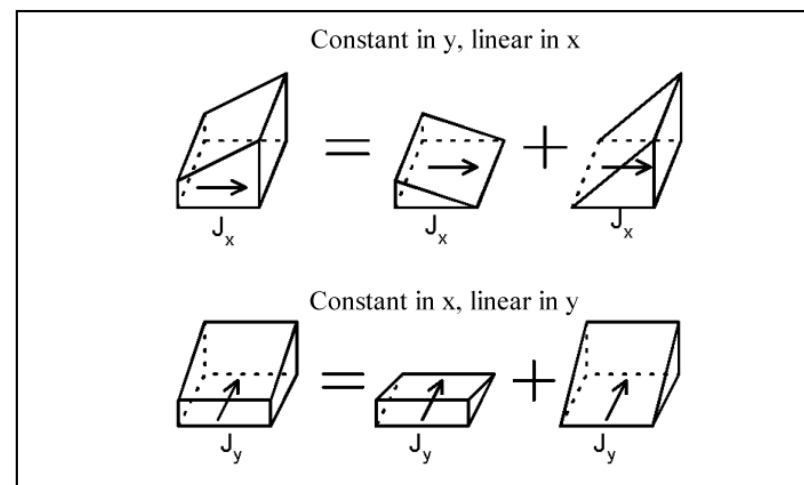
- Mesh is used to define rooftop approximating functions for the edge currents
- Amplitudes (f_0, f_1, f_2, \dots) are unknown and must be computed
- Current is assumed to vary along direction of travel and be constant across the other direction (think of how current moves on a TL)



the_06.gif

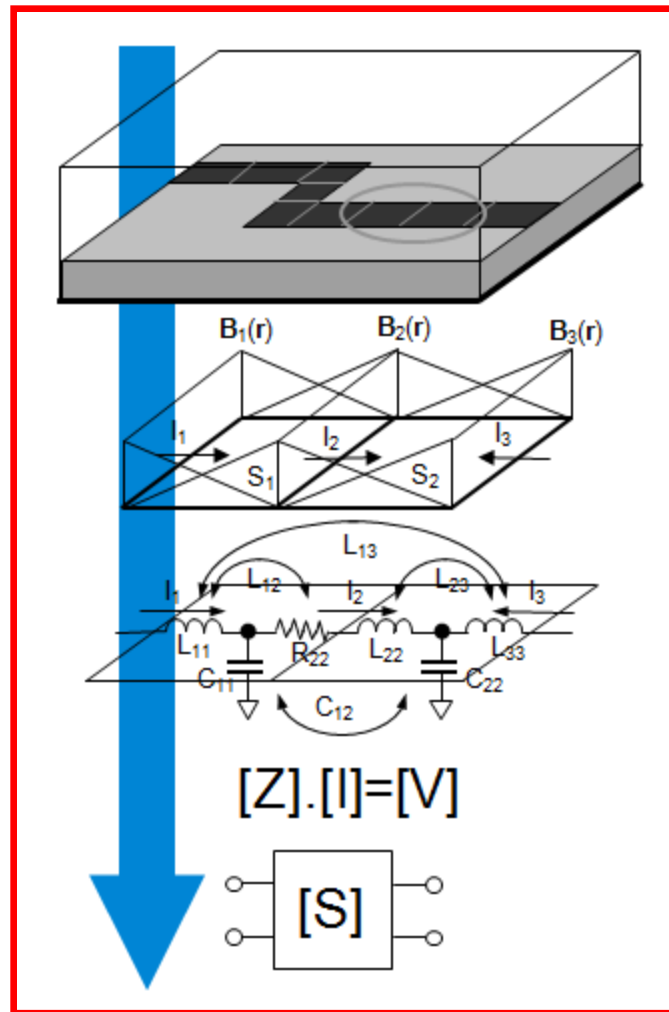


the_02.gif



the_05.gif

Full Wave Method of Moments – Momentum uWave



- Full wave electric & magnetic Green's functions

$$e^{-jk|\mathbf{r}-\mathbf{r}'|}$$

- MoM problem can be mathematically thought of as a **3D equivalent circuit network with frequency-dependent R's, L's, and C's**
- An **impedance matrix** is created and then solved that allows us to obtain the current amplitudes based on the excitations at the ports

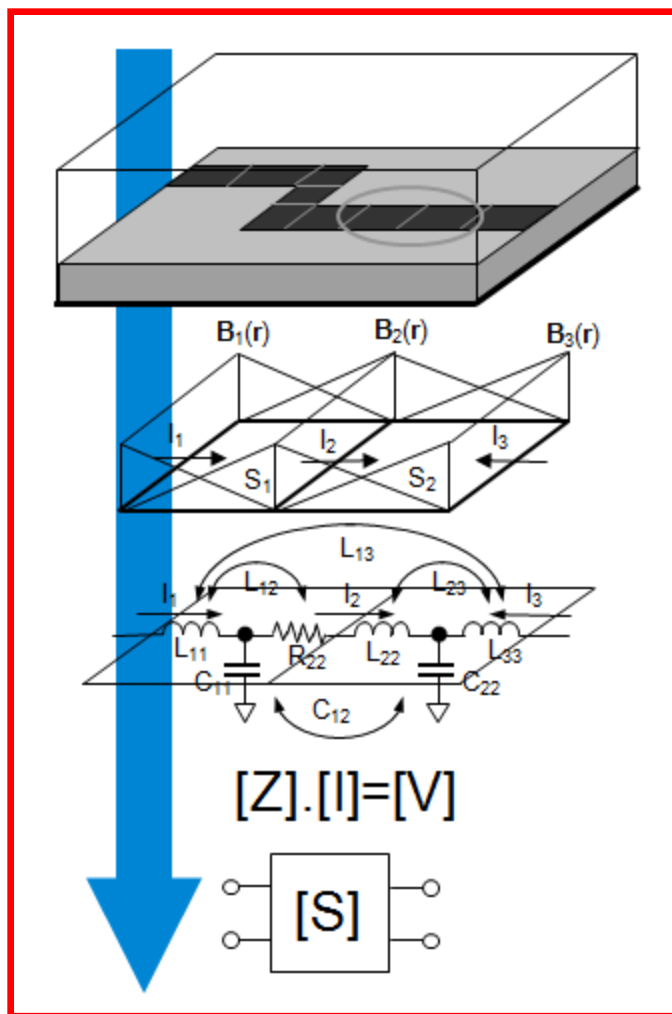
$$Z_{ij}^L = j\omega L_{ij}(\omega) = \iint_{S_i} dS \iint_{S_j} dS' G_m(\omega, \mathbf{r} - \mathbf{r}') \mathbf{B}_i(\mathbf{r}) \cdot \mathbf{B}_j(\mathbf{r}')$$

$$Z_{ij}^C = \frac{1}{j\omega C_{ij}(\omega)} = \iint_{S_i} dS \iint_{S_j} dS' G_e(\omega, \mathbf{r} - \mathbf{r}') \nabla \cdot \mathbf{B}_i(\mathbf{r}) \nabla \cdot \mathbf{B}_j(\mathbf{r}')$$

$$Z_{ij}^R = R_{ij}(\omega) = Z_s(\omega) \iint_{S_i} dS \iint_{S_j} dS' \delta(\mathbf{r} - \mathbf{r}') \mathbf{B}_i(\mathbf{r}) \cdot \mathbf{B}_j(\mathbf{r}')$$

See R. F. Harrington, *Field Computation by Moment Methods*. Macmillan, New York (1968).

Quasi Static Method of Moments – MomentumRF



Low Frequency approximation :

$$e^{-jk|\mathbf{r}-\mathbf{r}'|} \approx 1 - jk|\mathbf{r}-\mathbf{r}'|$$

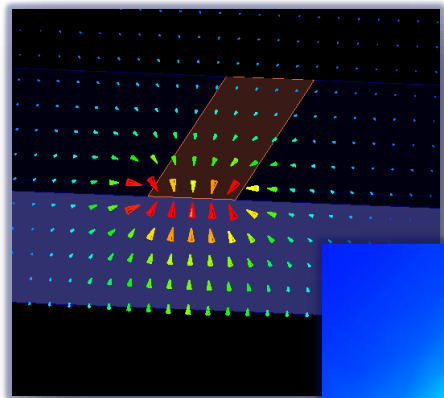
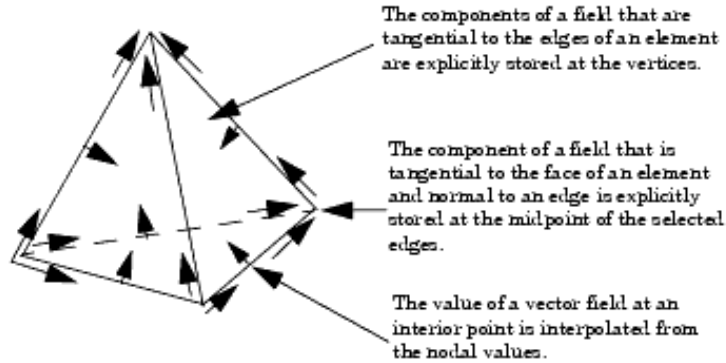
- Electro- and magnetostatic Green's functions
- Quasi-static frequency scaling ($j\omega$, $1/j\omega$)
- L's and C's are real and frequency independent
- R's are complex (DC loss + skin effect $\sqrt{\omega}$)

[Z] matrix load is frequency independent !

$$Z_{ij}^L = j\omega L_{ij} = j\omega \iint_{S_i} dS \iint_{S_j} dS' G_m(\mathbf{r}-\mathbf{r}') \mathbf{B}_i(\mathbf{r}) \cdot \mathbf{B}_j(\mathbf{r}')$$

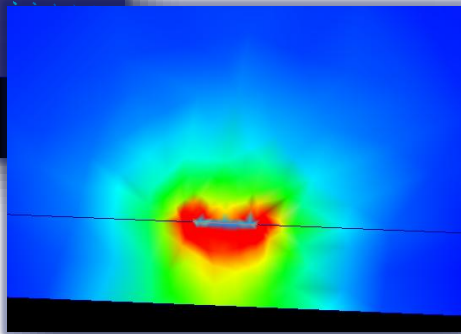
$$Z_{ij}^C = \frac{1}{j\omega C_{ij}} = \frac{1}{j\omega} \iint_{S_i} dS \iint_{S_j} dS' G_e(\mathbf{r}-\mathbf{r}') \nabla \cdot \mathbf{B}_i(\mathbf{r}) \nabla \cdot \mathbf{B}_j(\mathbf{r}')$$

$$Z_{ij}^R = R_{ij}(\omega) = Z_s(\omega) \iint_{S_i} dS \iint_{S_j} dS' \delta(\mathbf{r}-\mathbf{r}') \mathbf{B}_i(\mathbf{r}) \cdot \mathbf{B}_j(\mathbf{r}')$$



Excitation field

$$E = \text{Re}[E(x, y)e^{j\omega t - \gamma z}]$$



• 2D Problem to define the excitation

$$\nabla \times \left(\frac{1}{\mu_r} \nabla \times E(x, y) \right) - k_0^2 \epsilon_r E(x, y) = 0 \quad k_0 = \sqrt{\mu_0 \epsilon_0}$$

• Full 3D equation for E

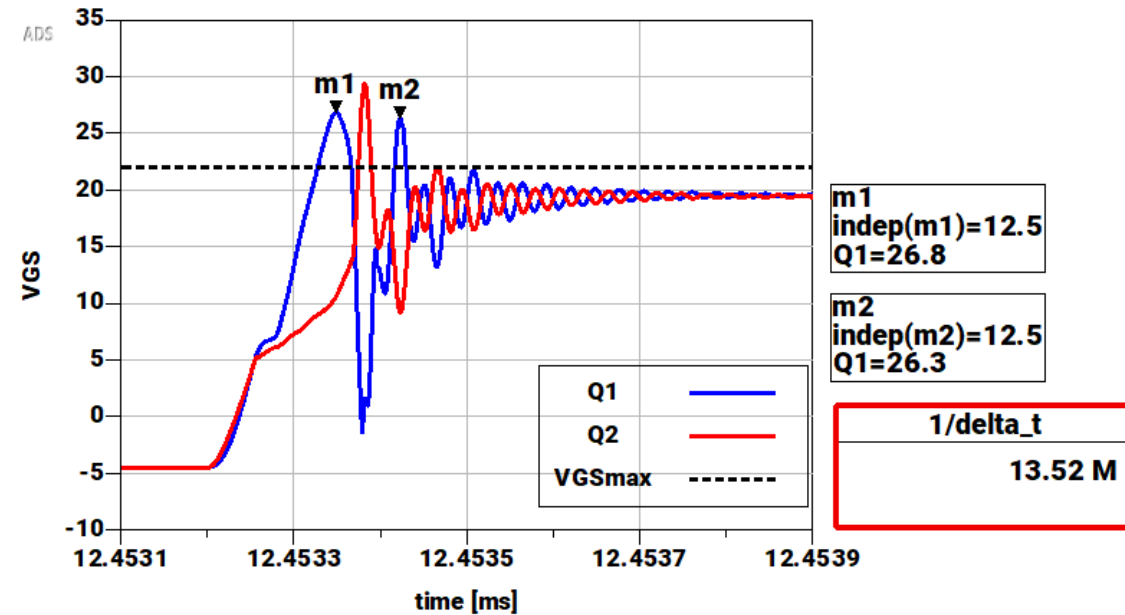
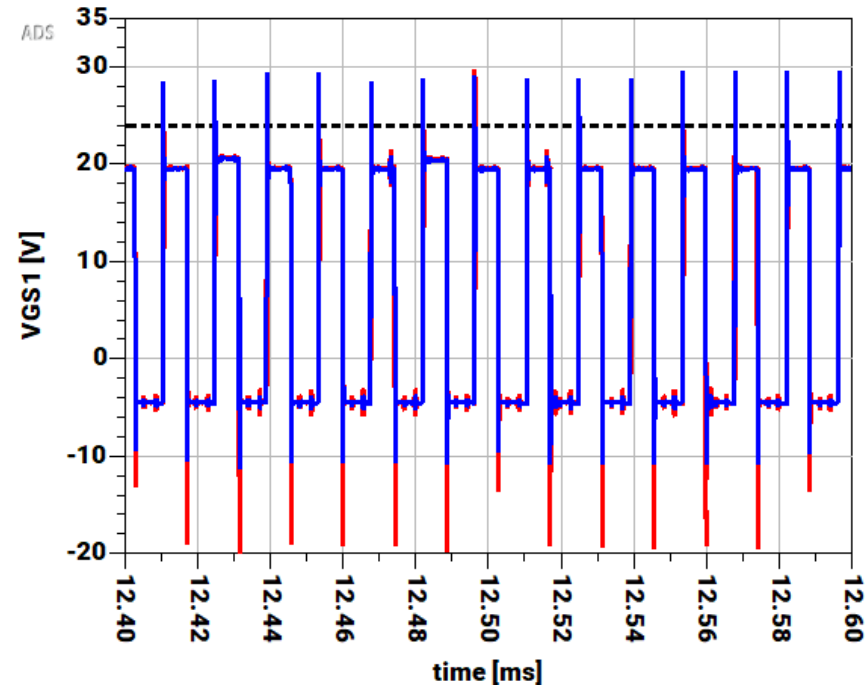
$$\nabla \times \left(\frac{1}{\mu_r} \nabla \times E(x, y, z) \right) - k_0^2 \epsilon_r E(x, y, z) = 0$$

• Multiply by the phasor to obtain the physical field

$$E(x, y, z, t) = \text{Re}[E(x, y, z)e^{j\omega t}] \quad H = \frac{\nabla \times E}{-j\omega\mu}$$

Simulation Results

Voltage Overshoot

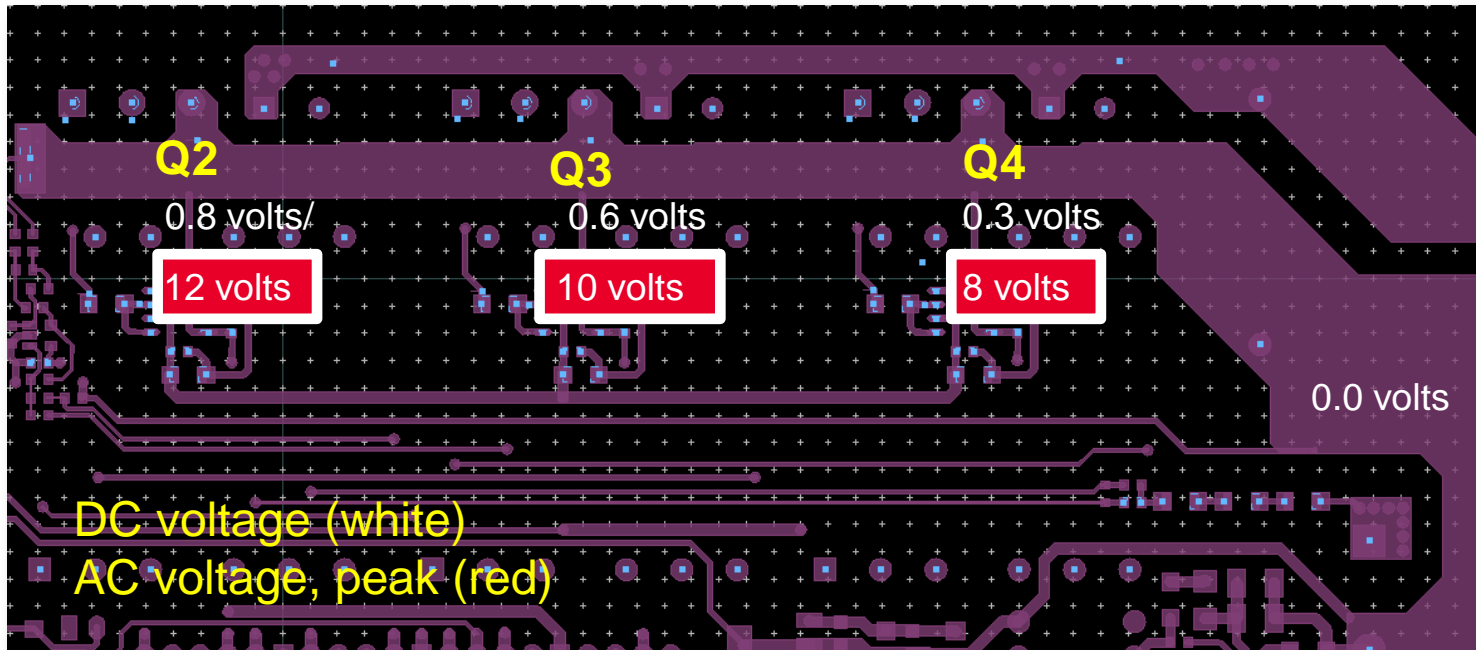


Palomba F., Gennaro F., Pavone M., Aiello N., Aiello G., Cacciato M.: Analysis of PCB parasitic effects in a Vienna Rectifier for an EV battery charger by means of Electromagnetic Simulations, **EPE'19 ECCE Europe ISBN: 978-9-0758-1530-6**



Simulation Results

Ground Bouncing

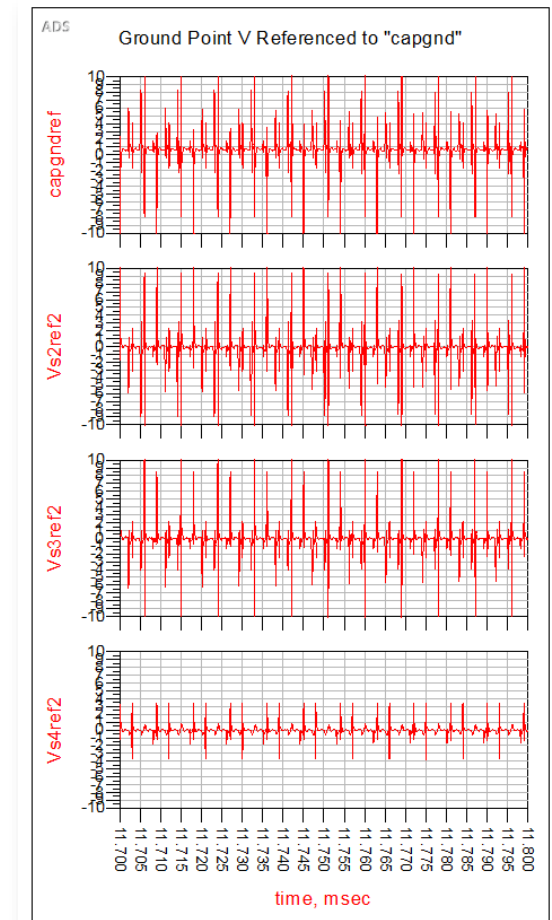


Root causes:

- Ohmic Losses - IR drop
- di/dt

Impact:

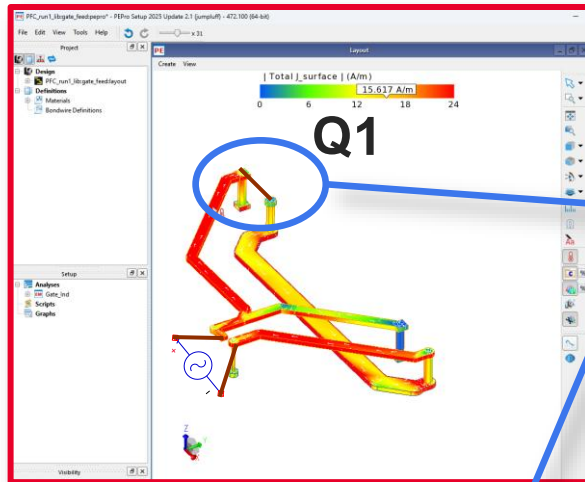
- Noise generation
- False Commutation
- Device failure



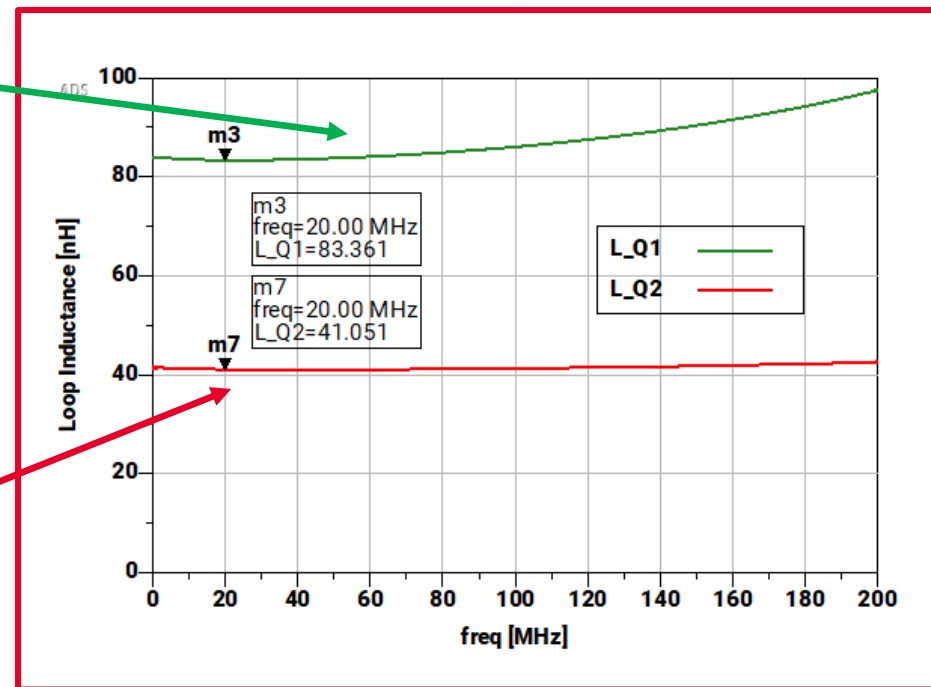
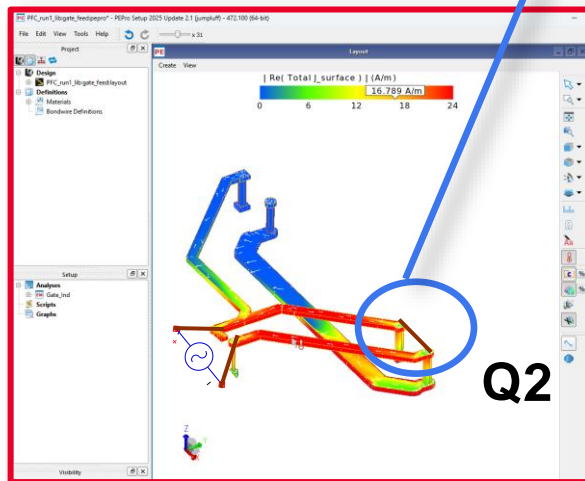
Simulation Results

Control Line Inductance

1. EM simulation of Control Lines
2. Replace the MOSFET with a short
3. Extract the Line Impedance from $S_{1,1}$



Ideal Short



$$Z_{trace} = Z_0 \frac{1 + S_{1,1}}{1 - S_{1,1}}$$

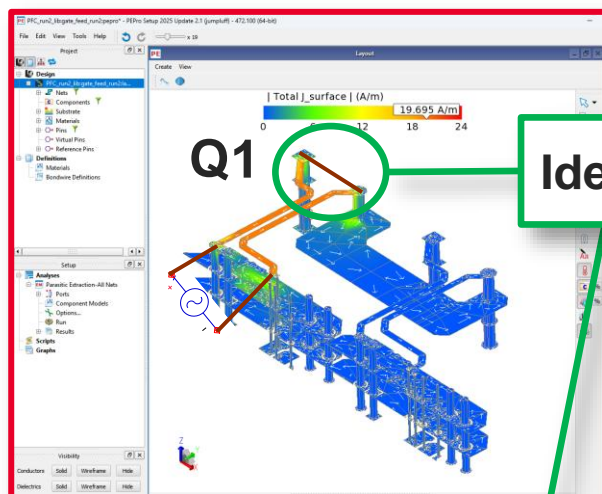
$$L_{trace} = \frac{Im[Z_{trace}]}{2\pi f}$$



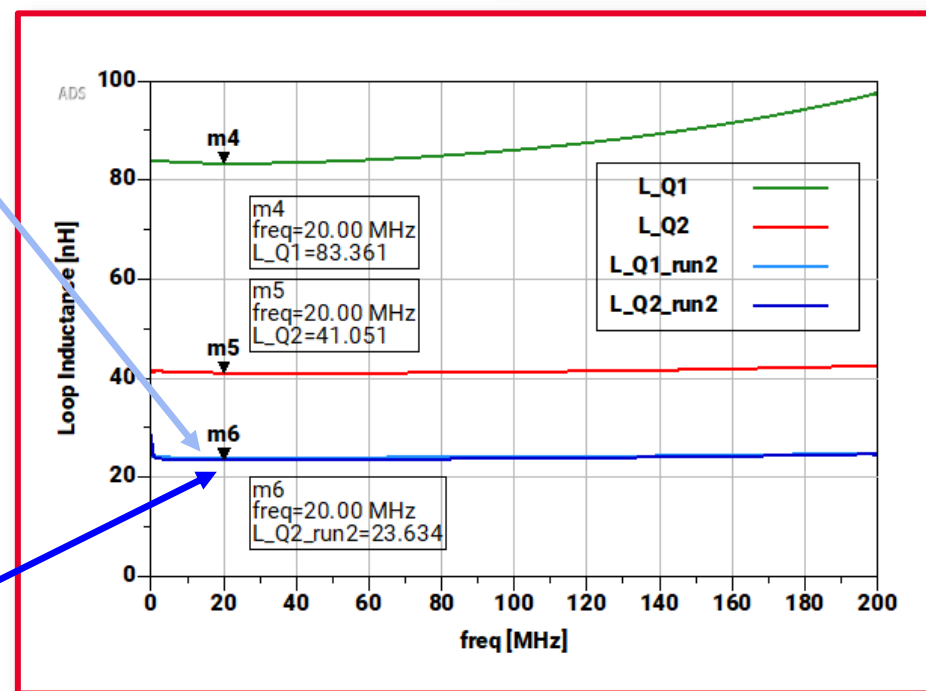
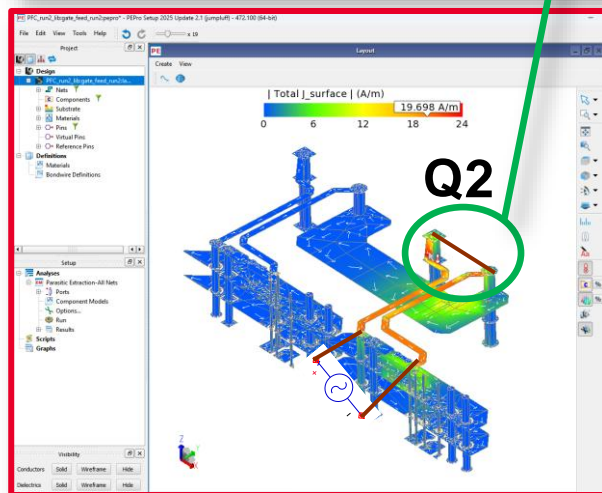
Simulation Results

Control Lines Inductance – Redesign

- Control Lines redesign to obtain:
 - Balanced Circuit
 - Lower Parasitic Inductance



Ideal Short



$$Z_{trace} = Z_0 \frac{1 + S_{1,1}}{1 - S_{1,1}}$$

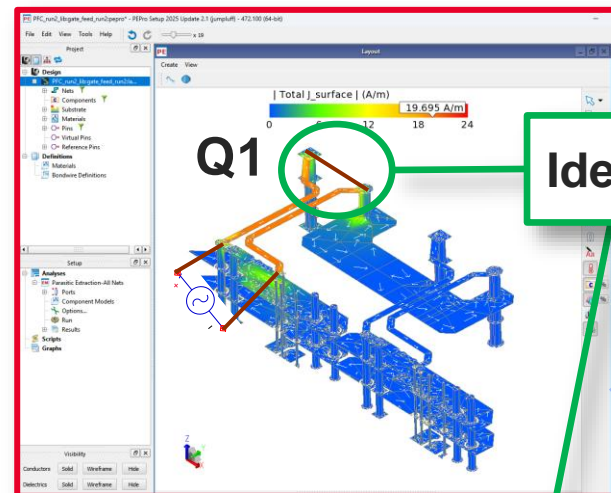
$$L_{trace} = \frac{Im[Z_{trace}]}{2\pi f}$$



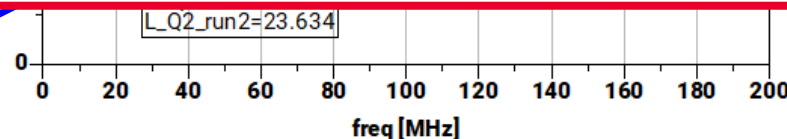
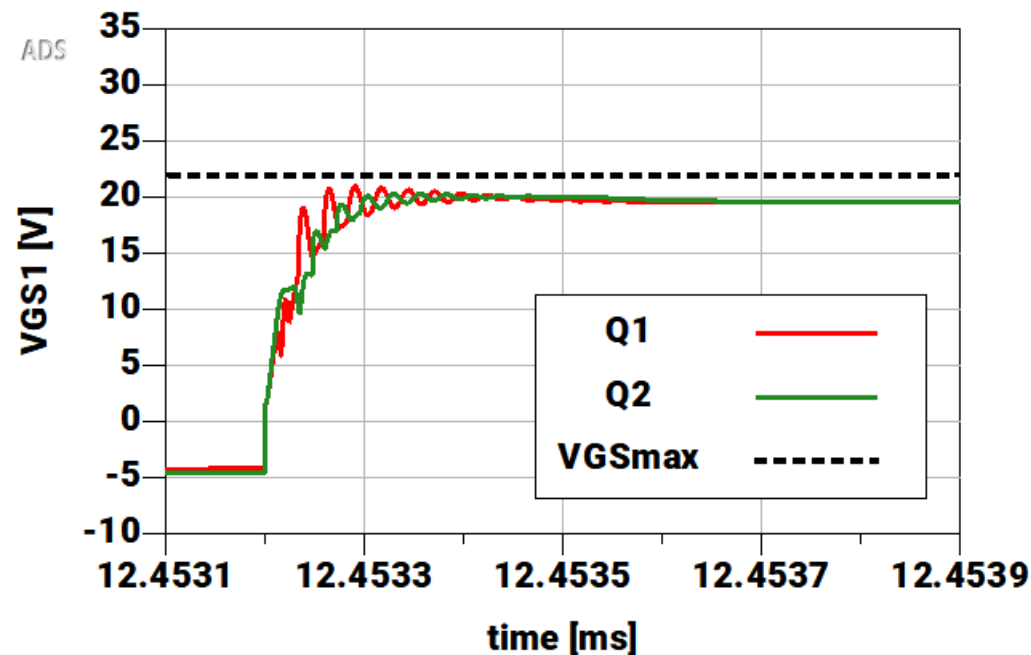
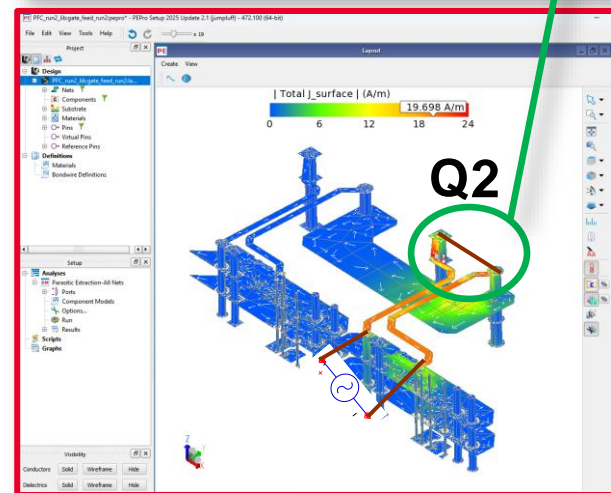
Simulation Results

Control Lines Inductance – Redesign

➤ Control Lines redesign to obtain:



Ideal Sh



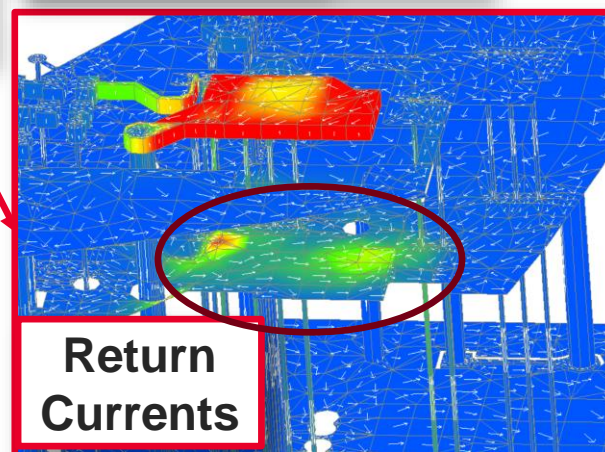
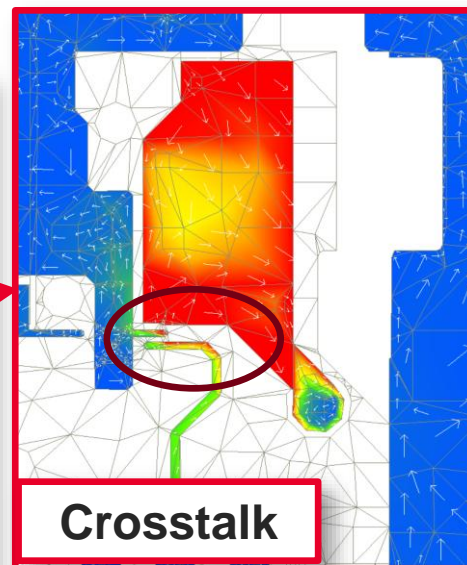
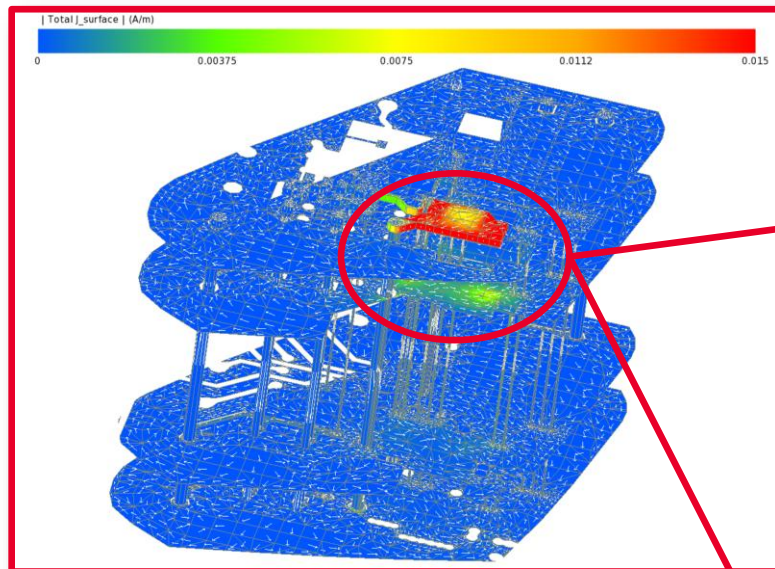
$$= Z_0 \frac{1 + S_{1,1}}{1 - S_{1,1}}$$

$$= \frac{Im[Z_{trace}]}{2\pi f}$$



Simulation Results

Crosstalk and Return Currents



Deep insight on

- Current distribution
- Coupled signals
- Return currents

**SPI 2025
BEST PAPER AWARD**

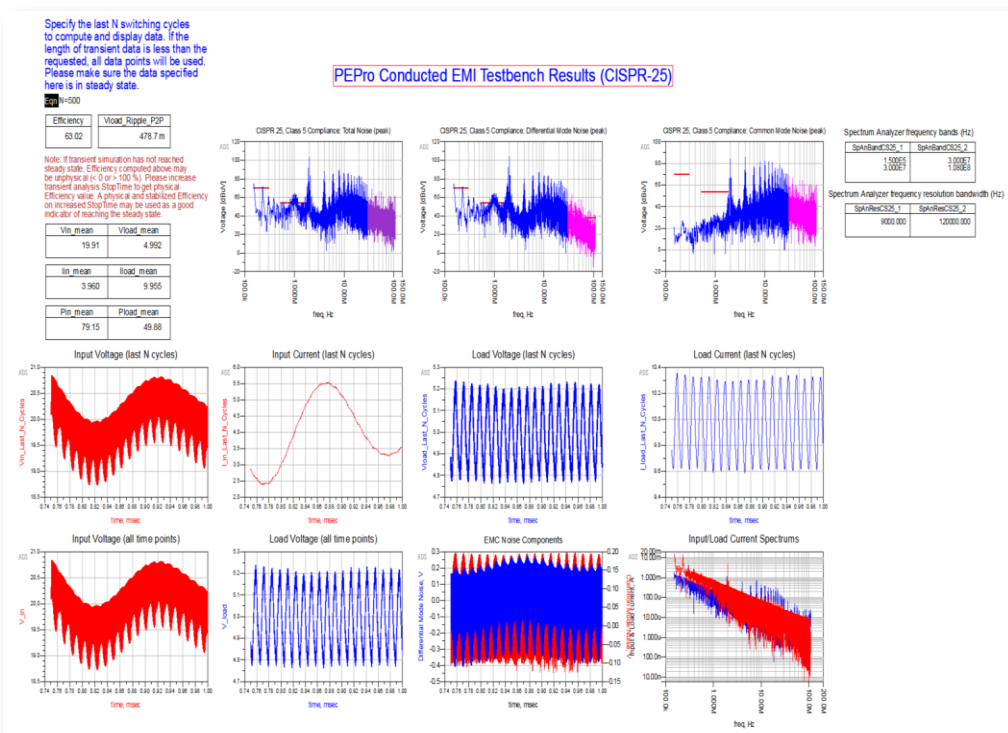


SESSION 7	
10:50 – 12:10	CROSS TALK & NOISE REDUCTION / MEMRISTORS Chair: Jose Schutt-Aine
10:50	Nicola Femia (1), Giulia Di Capua (2), Antonio Maffucci (2) (1) University of Salerno, Italy; (2) University of Cassino and Southern Lazio, Italy Power-to-Control Crosstalk in Power Electronic Circuits

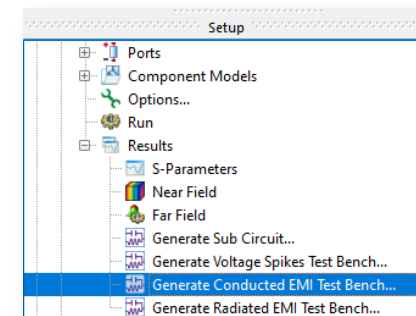
Simulation Results

Conducted EMI test

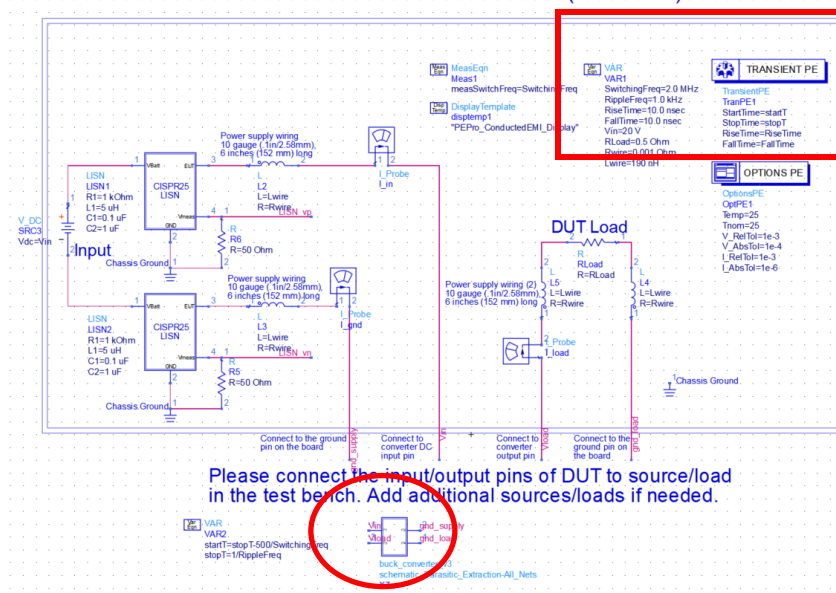
- Dedicated Analysis for Conducted EMI test
- SMPS noise calculated from the Linear Impedance Stabilization Network (LISN) output according to the CISPR-25.



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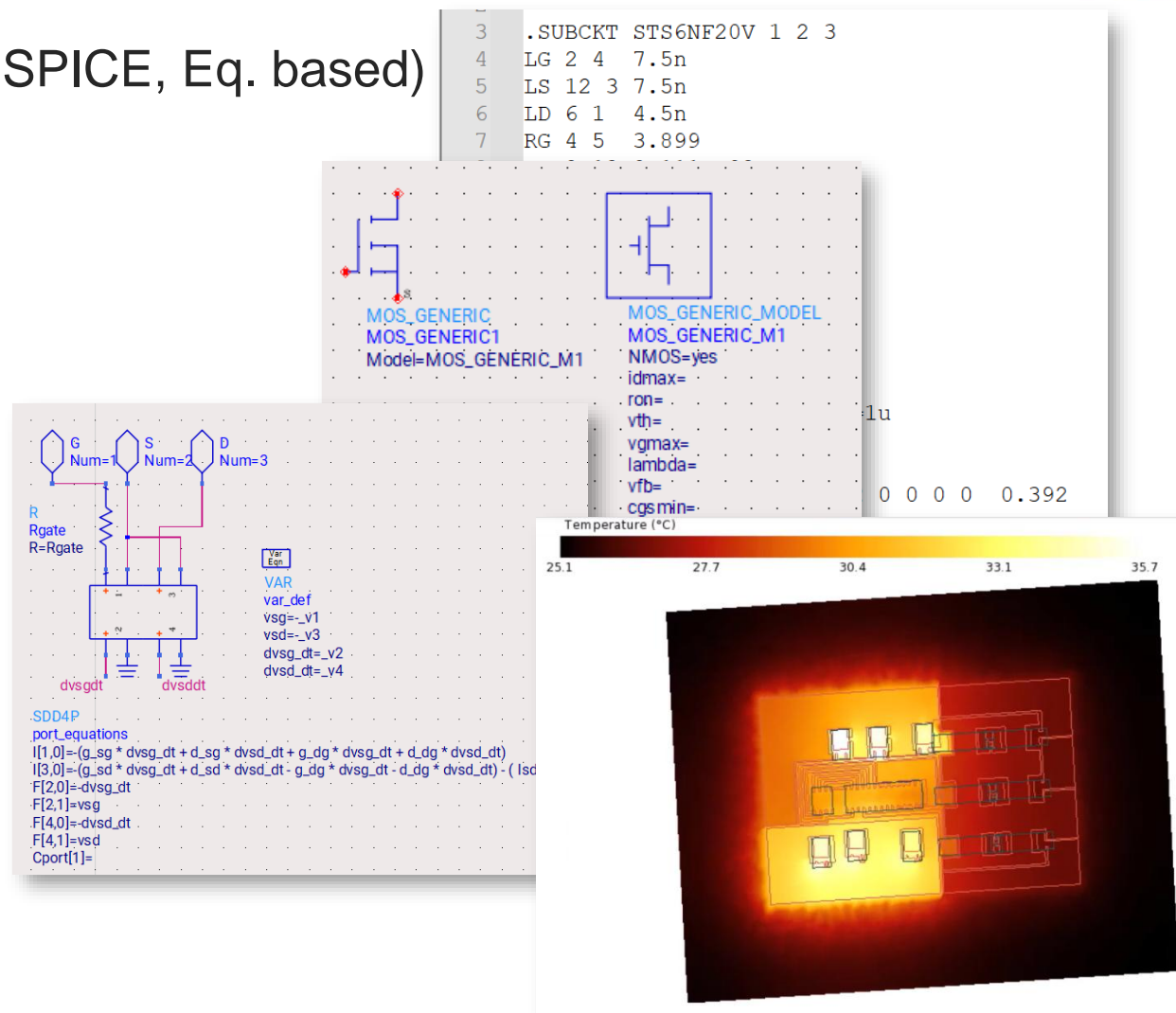
Conducted EMI Test Bench (CISPR 25)



The EM analysis result of the board and the mounted parts are automatically placed as a sub circuit.

Design challenges and Future Developments

- MOSFET/diode modeling (behavioral, SPICE, Eq. based)
- Modelling of Drivers and other PMIC
- S-par vs lumped models
- Low Frequency Extraction
- Thermal and Electrothermal Analysis
- Radiated EMI Simulation Accuracy
- Stability Analysis
- AI driven design





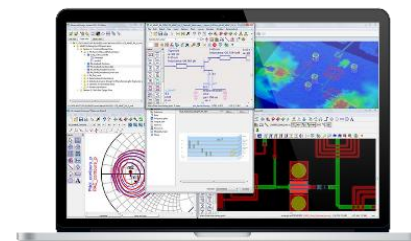
“All models are wrong, but some are useful”

George Box, 1976

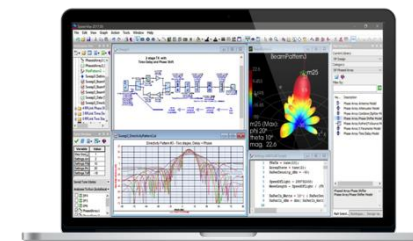
Keysight EDA University Program

Providing Industry-Grade Software to Support Universities

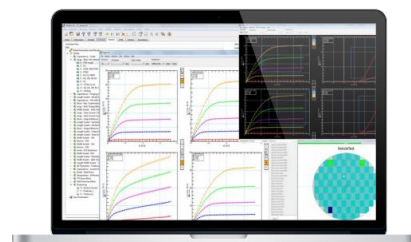
- Suite of EDA tools are used by top companies for
 - RF and Microwave, High-Speed Digital Design
 - Power Electronics Design and EMI Analysis
 - System-level Simulation
- Industry-leader with 65% market share¹
- Giving students access to industry-standard tools
 - **Provided at low cost to universities**
 - Students can request license for their computer
- To be 'industry-ready', students need to understand the full design flow
 - Design and simulation at the component / device level
 - Test and measurements
 - Easy to move through workflow using PathWave
- Works with Keysight's RF/Microwave and High-Speed Digital Student Certification Programs



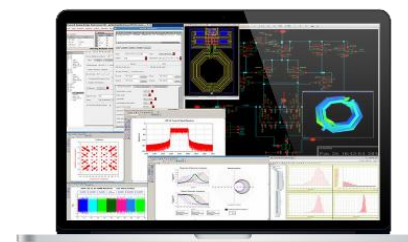
PathWave Advanced Design System (ADS)



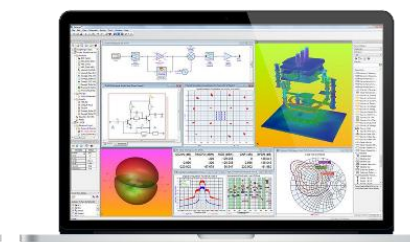
PathWave System Design (SystemVue)



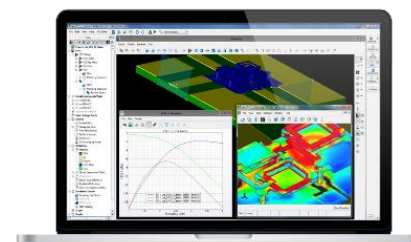
PathWave Device Modeling (IC-CAP, MBP, MQA)



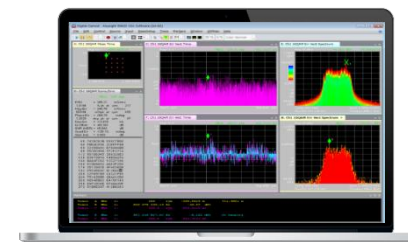
PathWave RFIC Design (GoldenGate)



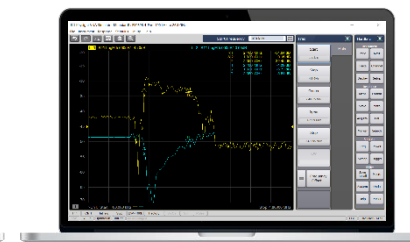
PathWave RF Synthesis (Genesys)



PathWave EM Design (EMPro)



PathWave Vector Signal Analysis (VSA)²



Keysight VNA Simulator (Standard, S94050B)²

¹Industry: RF Design and Simulation, Source: Pedestal Research (Jan. 2020)

²Not branded under 'PathWave Design', but application is part of PathWave Design University W2130UU bundle

Thank you